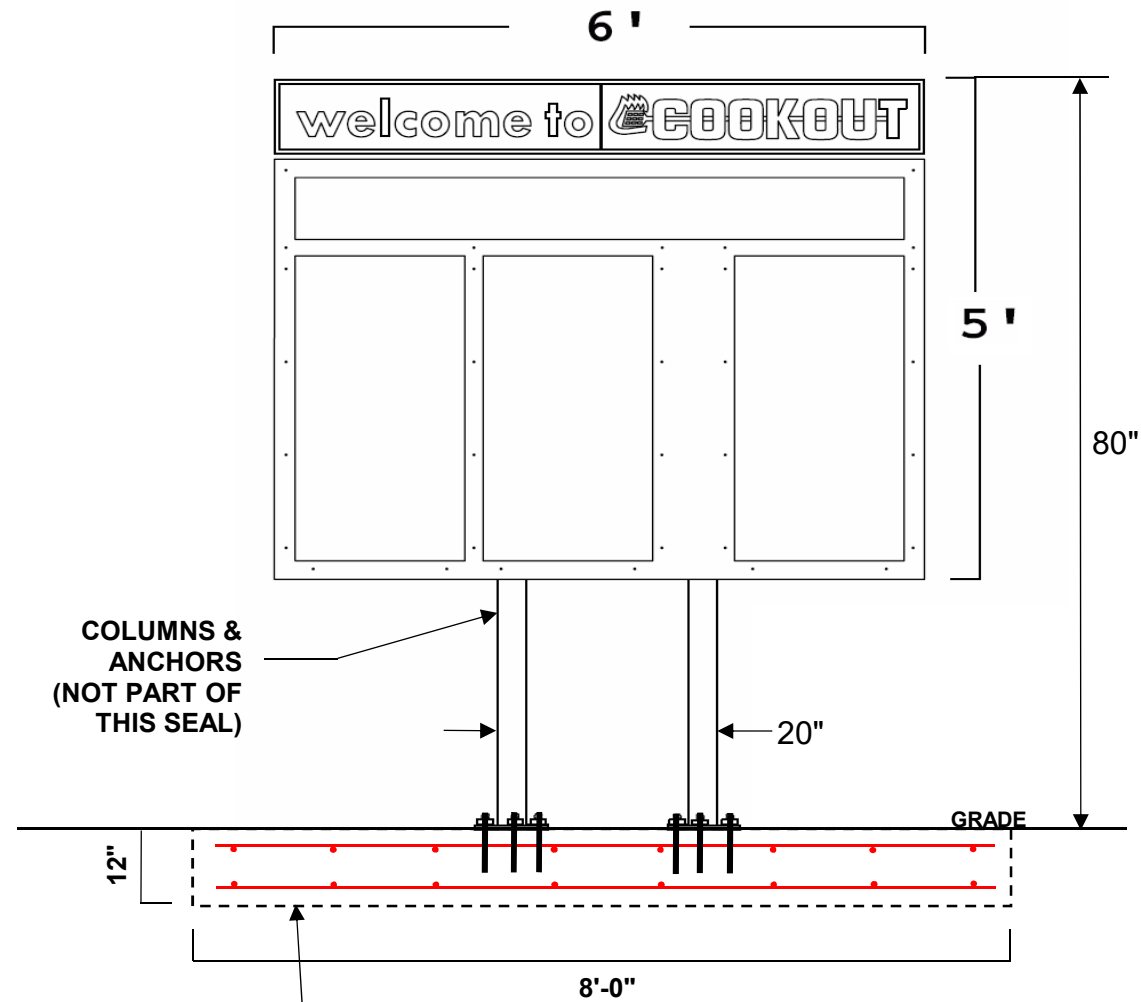


Sign Support Column



**4'-0" LONG x 8'-0" WIDE x 12" DEEP
SPREAD CONCRETE FOOTING w/ #5
REBAR AT 12" OC EACH WAY 3"
FROM TOP AND 3" FROM BOTTOM**

Spread Foundation (Long is perpendicular to face)
4' long x 8' wide x 1' deep
 #5, 12" OC each way, 2 mats, 3" from top and bot,
 gentle bend around column
 Weld 2' long 2x2x3/8 angle to bottom and side of
 column with 3/8 fillet weld all around
 All foundations: Embed column to 6" from bottom in
 2500psi concrete.

2015 INTERNATIONAL BUILDING CODE, Seismic D

ref ASCE7-10, Seismic Category D, Wind controls lateral load structural
150 Wind Speed, Vult, mph, from ASCE7-10, Figure 26.5
II Risk Category; II, Normal; III, Substantial Hazard; IV, Essential/Critical
C Wind Exposure; C, House size obstructions for 1200ft; D no obstructions

WIND LOAD CALC: ASCE 7-10, Sec. 29.4.1, Solid Freestanding Signs
 Terrain $K_{zt}=1$, no hill, ridge, or escarpment >15' high; Directionality $K_d=.85$; Gust $G=.85$ rigid
 structure; Wind Velocity $V_{asd}=\sqrt{V_{ult}^2 \cdot 6}$; $K_z=2.01 \cdot (H/900)^{(2/9.5)} \cdot \text{Exp} C$, $(700 \leq H \leq 11.5) \cdot \text{Exp} D$;
 $Q_{hasd}=.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V_{asd}^2$; $P_{asd}=Q_{hasd} \cdot G \cdot C_f$; $F_{seg}=P_{asd} \cdot W \cdot H$

116	Wind Speed, V_{asd} , mph	1.55	Force Coefficient, C_f		
A	B	C	D	E	F
6.7	1.7				Sign Segment ID
6.0	1.7				Segment Top Above Grade, Top, ft
5.0	1.7				Segment Width, W, ft
					Segment Height, H, ft
30	2.7556				Segment Area, ft ²
0.85	0.85				Velocity Pressure Exposure Coeff: K_z
24.9	24.9				Velocity Pressure, Q_{hasd} , psf
32.9	32.9				Wind Pressure, P_{asd} , psf
1.0	0.1				Segment Force, F_{seg} , kips
1.2	0.0				Load Case 2 Force, $F_2 = F_{seg} \cdot .2 \cdot W$
		1.3 ft OC	Column Spacing		
		1.1 kip	Total Shear at Grade, $V = \text{Sum}(F_{seg})$		
3.88		4.2 kip.ft	Total Moment at Grade, $M = \text{Sum}(F_{seg} \cdot (\text{Top}-H/2))$		
		1.4 kip	Column Shear, $V_c = V/2 - \text{Sum}(F_{seg} \cdot 2 \cdot W) / \text{Spacing}$		
1.35		5.6 kip.ft	Column Moment at Grade, $= \text{Sum}(F_{seg} \cdot (\text{Top}-H/2))$		

- Sign manufacturer/installer's design, detailing, fabrication, and erection shall conform to the following specifications: Building Code, ASTM specifications, ACI-318 for reinforced concrete, American Welding Society Code for Welding in Building Construction, AISC Specification for Design, Fabrication, and Erection of Structural Steel for Buildings.
- Materials of construction: (Unless noted otherwise)
 - Structural steel (angles, shapes, plates, gussets): ASTM A-36, $F_y = 36$ ksi.
 - HSS round steel tubing: A-500, Grade B, $F_y = 42$ ksi; Rectangular: 46ksi.
 - Structural aluminum tubing: 6053, 6061-T6, or equivalent, $F_y = 18$ ksi at weld.
 - Structural pipe: A-53, Grade B, Type E or S, $F_y = 35$ ksi.
 - Anchor bolts: ASTM F1554 Grade 36 with heavy hex at bottom, not "L or J" bolts.
 - Connection bolts: A-325, snug tight.
 - Rebar: ASTM 615, #6 or larger - Grade 60, #5 or smaller - Grade 40, 3" cover.
 - Concrete: 2500 psi, 28 days.
 - Provide coatings to prevent any possibility of corrosion.
- Welding design and fabrication according to AWS D1.1.
 - AWS certification required for all structural welders.
 - E70XX electrodes for SMAW processes. F7X-EXXX electrodes for SAW processes.
- Embedded column acts as vertical reinforcement for drilled and cube foundations.
- Soil must be verified by sign installer. This design assumes presumptive soil bearing capacity (asd) from 6th Ed FBC, Table 1806.2 (or IBC). Vertical = 1500 psf for Class 5 (clay/silt CL,ML,MH,CH), Lateral = 2*150 psf/ft for Class 4 (sand, silty sand, clayey sand, SW,SP,SM,SC,GM,GC), and Lateral Sliding Coeff = .25 for Class 4 soil. Lateral brg is doubled for sign poles per 1806.3.4. If there is a question about soil bearing do a soil test.

Cube Drilled Shaft Foundation

L=W=D 6th Ed FBC, 1807.3.2.1, No lateral constraint at grade

	Diameter, b, ft	(or length and width of cube)
	Depth, D, ft	$D = .5 \cdot A \{ 1 + [1 + (4.36 \cdot H_{cent}/A)]^{.5} \}$
A		$A = 2.34 \cdot F / (S1 \cdot b)$
S1		$S1 = 2 \cdot S_{sand} \cdot D/3$

Spread Foundation

- 4.0** Length, L, ft
- 8.0** Width, W, ft
- 1.0** Depth, D, ft
- 1950 Soil Bearing at Bottom of Fdn, Q_{bot} , psf, $Q_{bot} = 1.3 \cdot (Q + 100 \text{pcf} \cdot (D-1))$
- 4.8** Total Weight, Wt, kips, $Wt = L \cdot W \cdot D \cdot .15$ kips/ft³
- 0.6** Toe Length, Toe, ft, $\text{Toe} = Wt / (W \cdot Q_{bot})$
- 1.8** Bearing Eccentricity, e, ft, $e = L / 2 - \text{Toe} / 3$
- 5.7** Overturning Capacity Calc, OT, kip.ft, $OT = Wt / e / 1.5 \text{ safety}$

MARK DISOSWAY, PE
 disoswaydesign@gmail.com
 163 SW Midtown Place, Ste 103
 Lake City, Florida 32025
 386-754-5419

SCPE21825

6/14/2018

This seal for structural engineering
 (Foundation & Support Column ONLY)

SCOPE OF WORK: Design sign support column and foundation to meet structural requirements of building code based on stated (not verified) site factors and size & shape based on sign installer's drawing, attached.

By using this engineering the owner, manufacturer, and installer accept responsibility to: Design, build, and install sign cabinet, face, attachment, electrical, etc according to sign code, building code, and UL. Verify site conditions match stated wind speed, risk, exposure, topo, and soil factors.

**Brandrite Sign
Company Inc.**

JOB#

PYLON SIGN
 2 Columns,
 Embedded in Foundation

Cookout
 8475 Dorchester Rd
 North Charleston, SC

Valid for one sign at this location.